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STATIC LOADING OF THE TM-46/MVM MINE-FUZE COMBINATION

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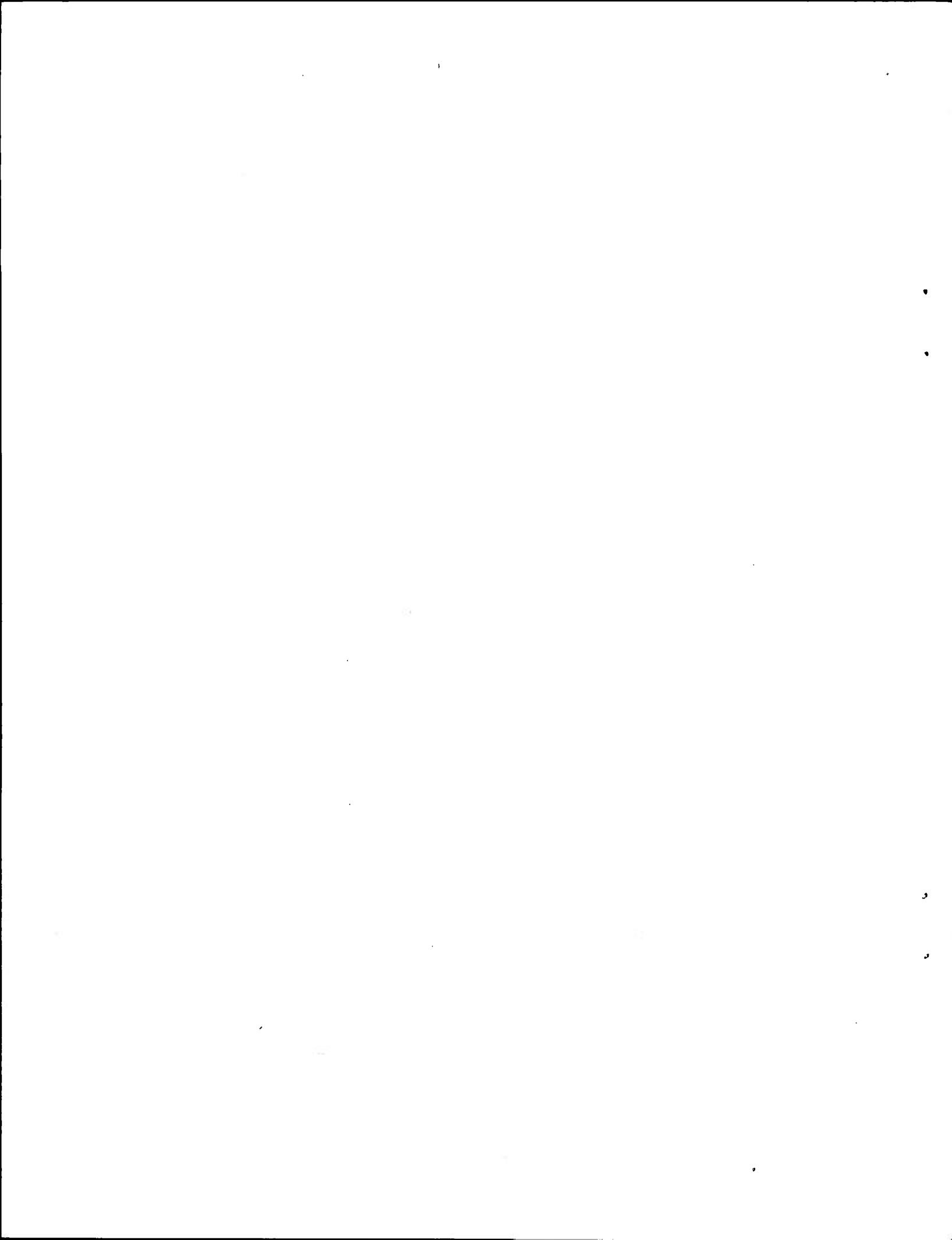
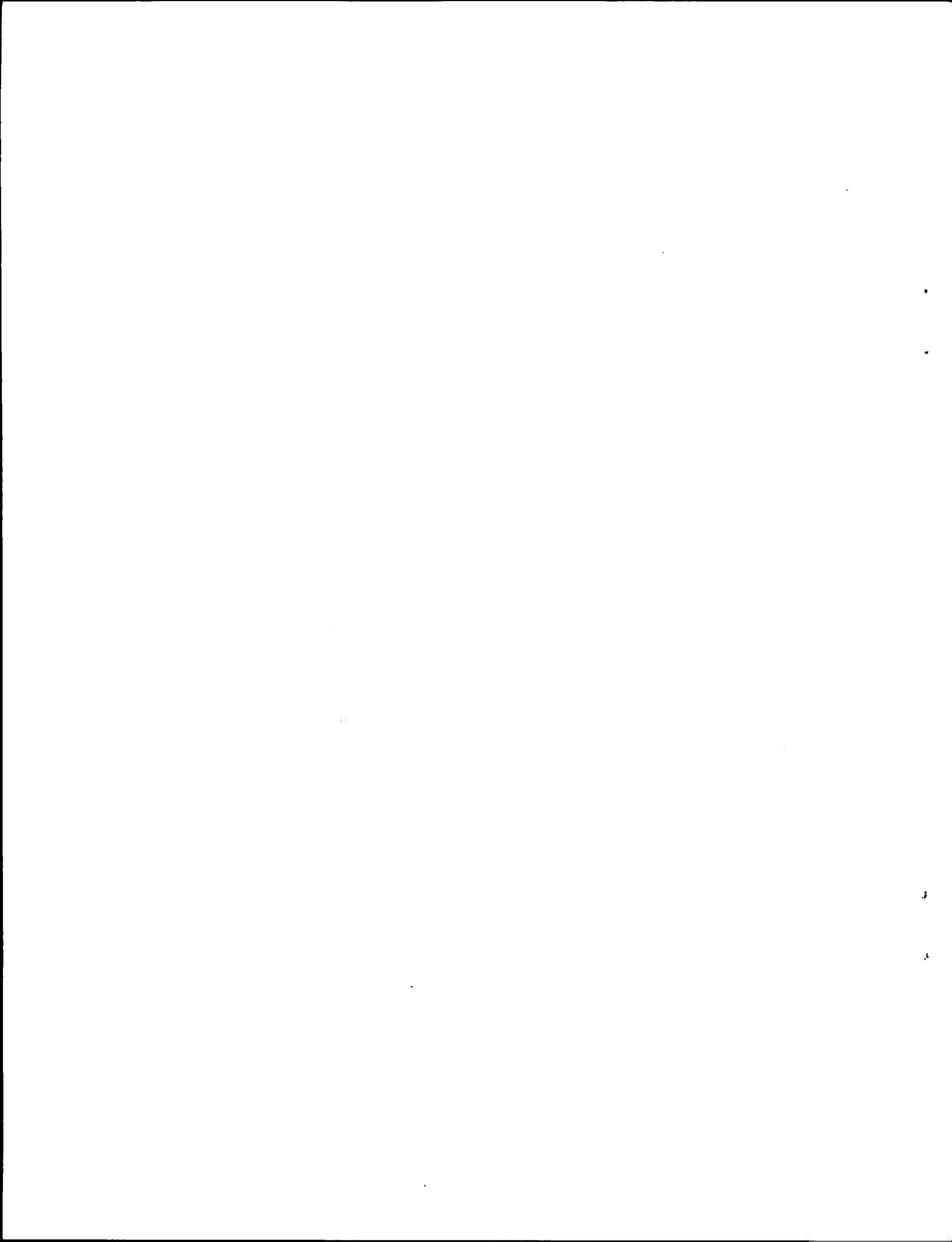


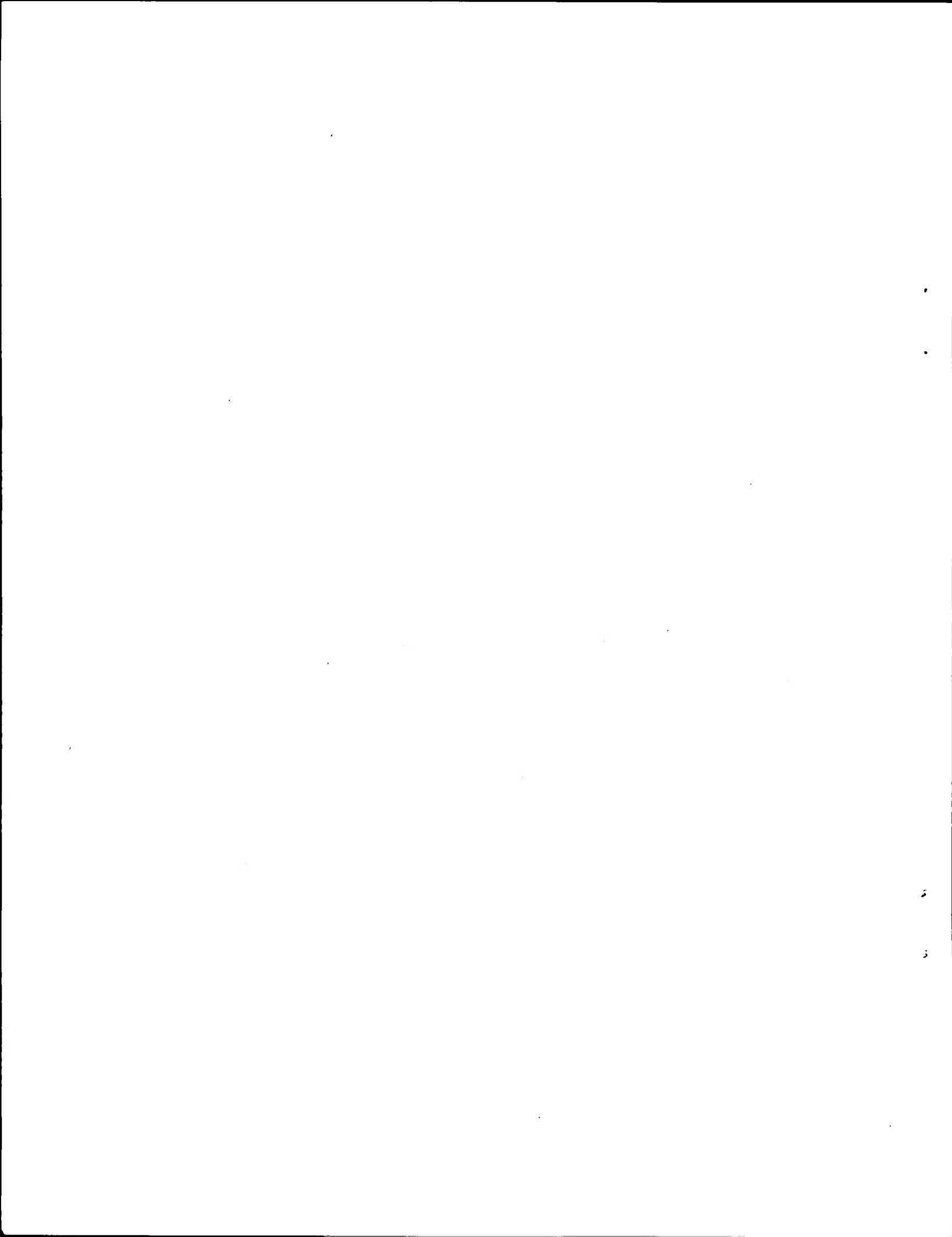
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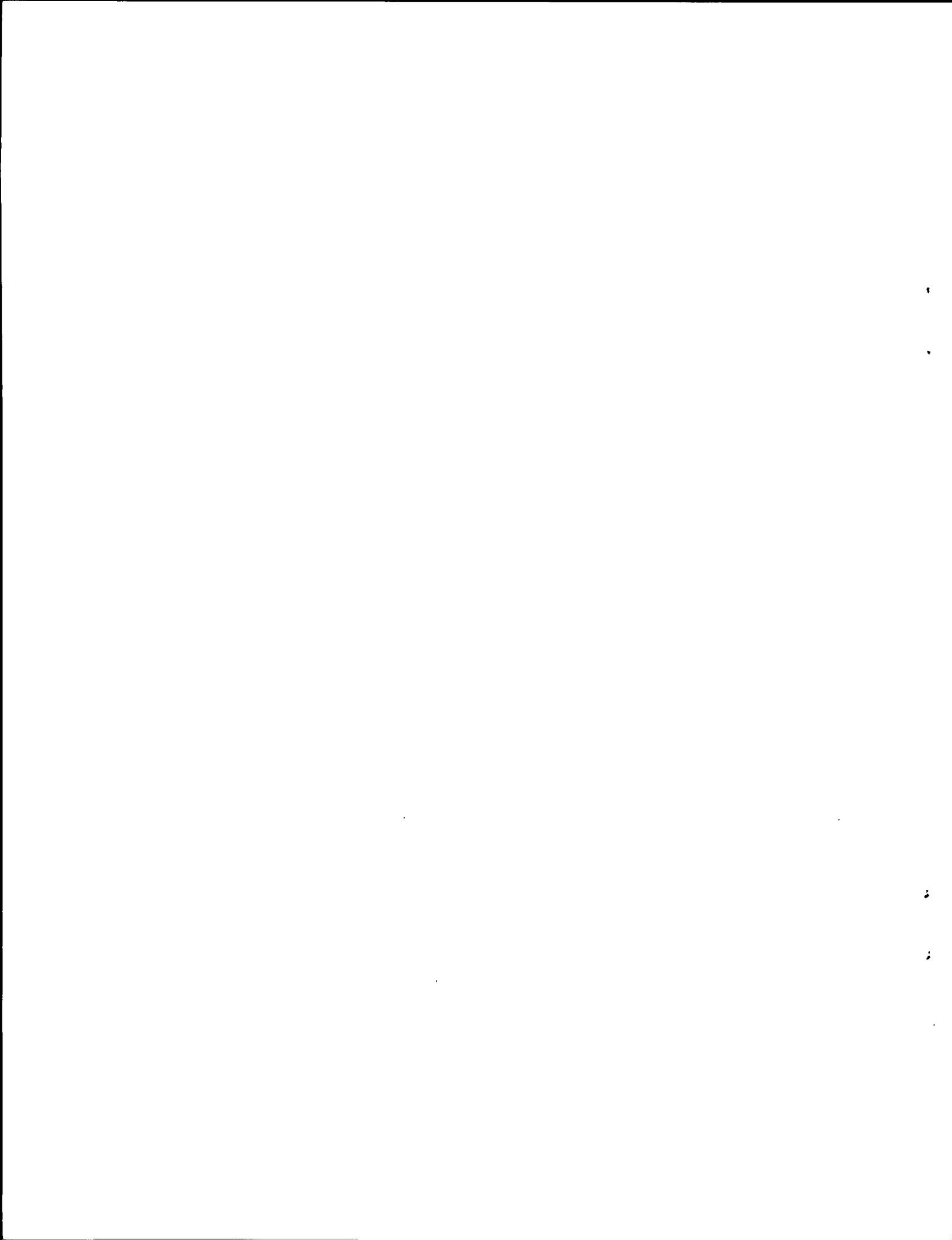
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I. INTRODUCTION

In order to establish a numerical model to assess the vulnerability and actuation characteristics of an anti-tank mine, it is necessary to have available an accurate method of determining the static load-deflection of the mine-fuze combination being studied. This is normally obtained from a standard-type load machine if the sensitive area is small or has a stiff pressure plate as in the M-15 anti-tank mine. However, for a large and irregular sensitive area, such as the TM-46 mine top, as shown in Figure 1, a loading method is needed which will equally load the entire top.

This report describes a way to uniformly load a mine of this type, the TM-46/MVM, and to measure the deflection of the top and to determine the fuze actuation pressure level. This technique combined with those of References 1 and 2 should give a quite accurate assessment for a given anti-tank mine.

II. TEST PROCEDURE

The test procedure describes the preparation of the mine, the static load generator, and the instrumentation used.

A. Mine Preparation

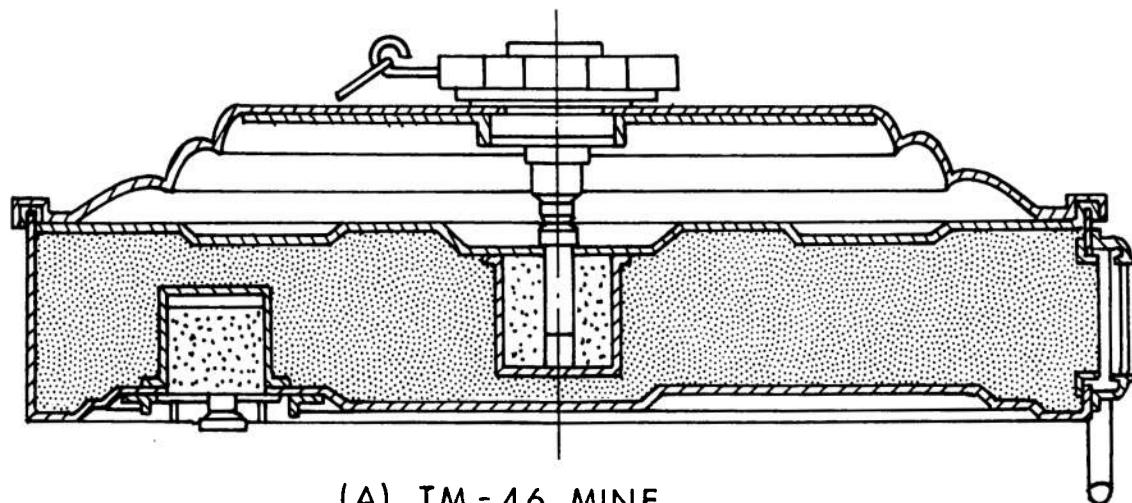
An inert TM-46 Russian anti-tank mine as shown in Figure 1, and an inert Model MVM pressure fuze with an extension tube from the MV-5 fuze as shown in Figure 2 were chosen for the deflection-load test. A small wire was silver soldered to the movable part of the fuze before installing it in the mine. A small clearance hole was drilled in the bottom plate of the mine to allow the wire attached to the fuze to extend through the end-plate of the test chamber. See Figure 3. A black paper target was attached to the fuze wire after the mine was clamped snugly at the end of the test chamber.

The deflection of the top of the mine/fuze combination when loaded with air pressure was observed by the corresponding movement of the attached paper target.

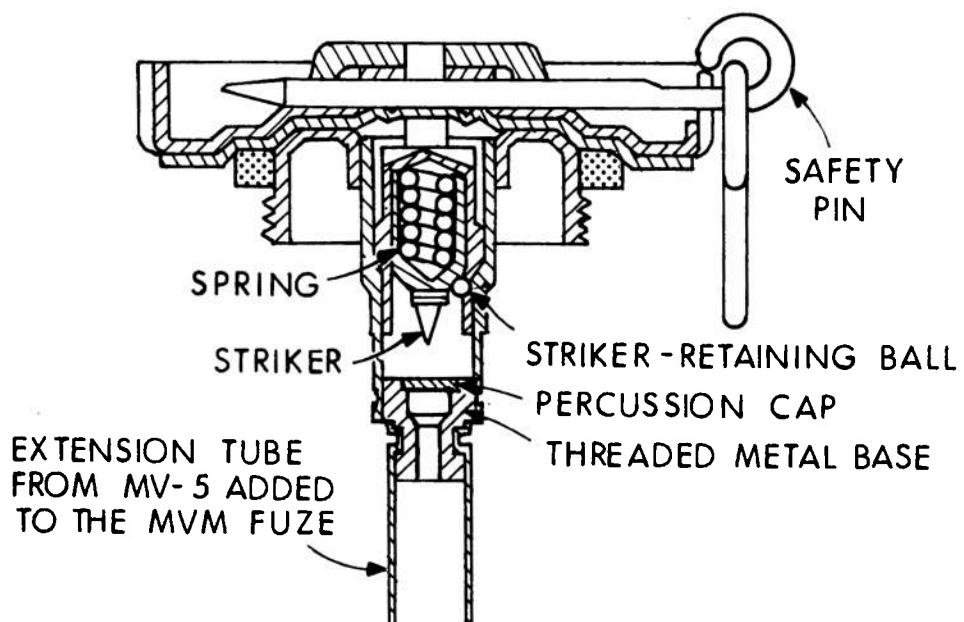
Details of the test set-up are given in Section B. below.

¹ Andrew Mark, "M-15 Anti-Tank Mine Vulnerability", BRL Tech Report ARBRL-TR-02211, January 1980. (AD #A080999)

² Charles Kingery, "Mine Actuation Tests", BRL Tech Report ARBRL-TR-02210, January 1980. (AD #B044271)



(A) TM - 46 MINE



(B) MVM FUZE ASSEMBLY

Figure 1. TM-46 mine and MVM pressure fuze.

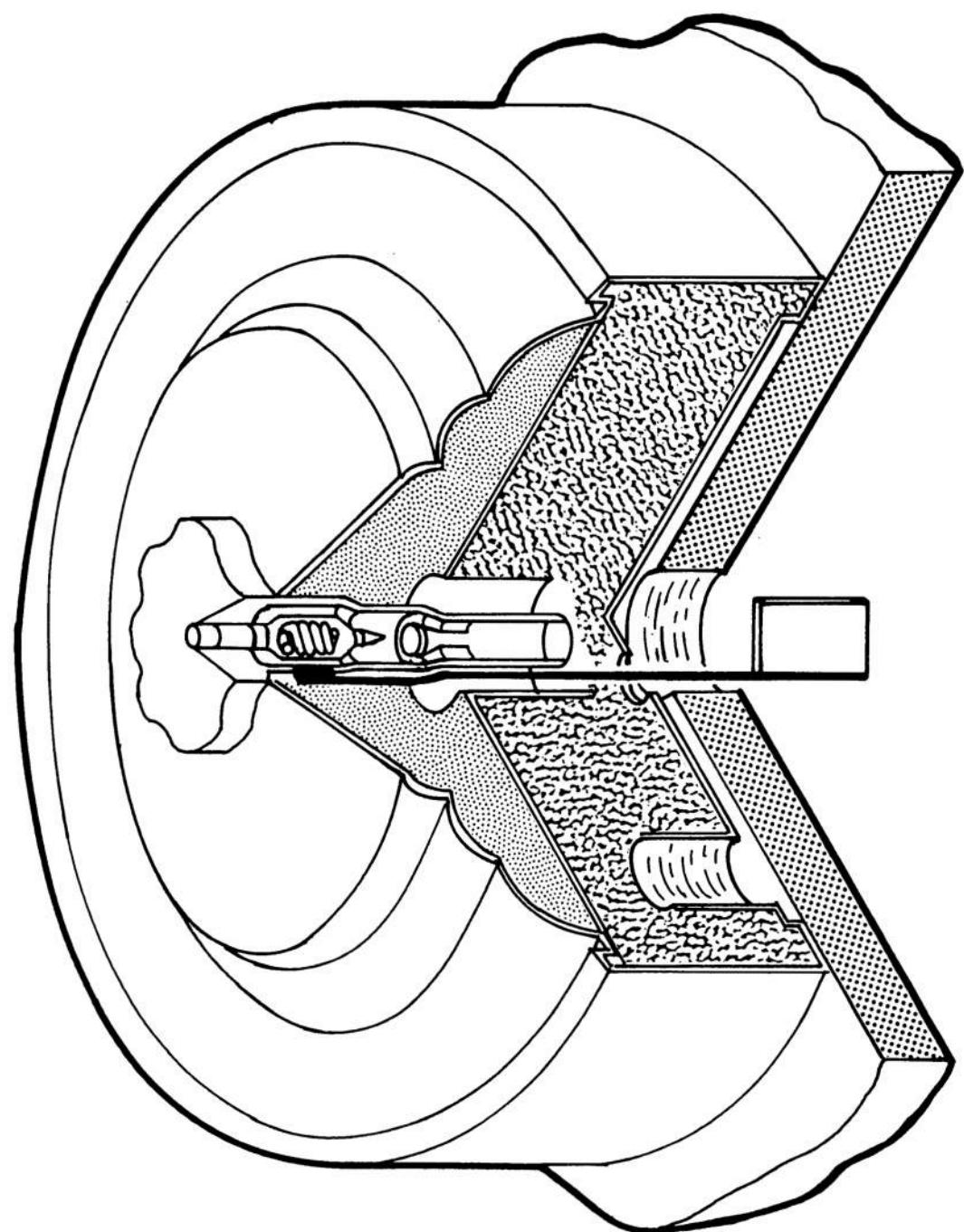


Figure 2. Mine-fuze with wire and optical target.

B. Static Load Generator

The static load generator used was adapted from the shock tube used in the mine actuation tests of Reference 2, Section I, above. Figure 3 shows how slight modifications were made. The principal changes were to shorten the test section and to close the driver section without the normal diaphragm.

The load was applied to the entire sensitive mine top at the end of the test chamber. Air was allowed slowly into the chamber through a regulator and monitored as the pressure was applied.

Details of the instrumentation are described in the next section.

C. Instrumentation

Figure 4 shows in schematic form the data acquisition-reduction system.

Three types of monitors were used to obtain the load-deflection data. The pressure transducer was a Tyco-Bytrex HFG50 of the strain-bridge type, with DC response. A second, Susquehanna ST-2 crystal transducer, was pressed and attached against the side of the mine where it acted as a vibration pick-up. It recorded the triggering of the fuze firing pin during the test. The third monitor was the optical displacement follower³, Optron 501, which observed the top deflection of the mine-fuze combination.

The Model 501 is designed to track a discontinuity in the intensity of the light reflected or emitted from a target surface. The lens system is used to focus the target discontinuity onto the photo cathode of an image dissector tube. Electrons are emitted from the back side of the photo cathode proportional to the intensity of the projected light. The electrons are accelerated to refocus on an aperture plate. The electrons are then collected to give a current output proportional to the number of electrons entering the aperture. The optical image is changed in this manner to an electron image - the current output is proportional to the corresponding incoming light intensity. The intensity in turn depends on the target (mine/fuze combination) movement into the illuminated field of view.

The voltage outputs from all three test monitors were suitably conditioned, amplified, and recorded with a 7600 Honeywell FM recorder. The remainder of the schematic in Figure 4 illustrates the data reduction system used to prepare the records obtained from the test.

³See company manual "Model 501 Optical Displacement Follower", Optron, Division of Univ. Tech. Inc., 30 Hazel Terrace, Woodbridge, Conn. 06525.

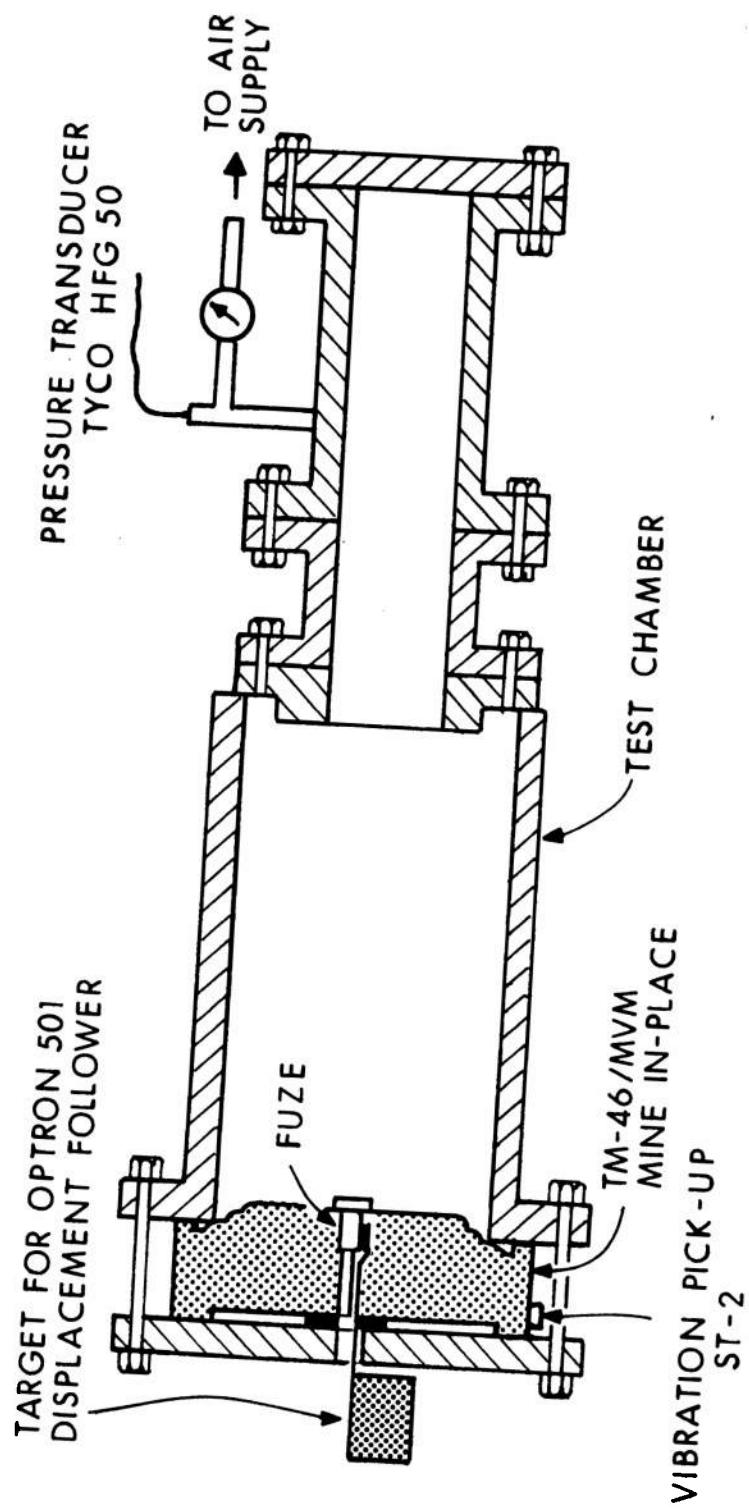


Figure 3. Experimental set-up for static load measurements.

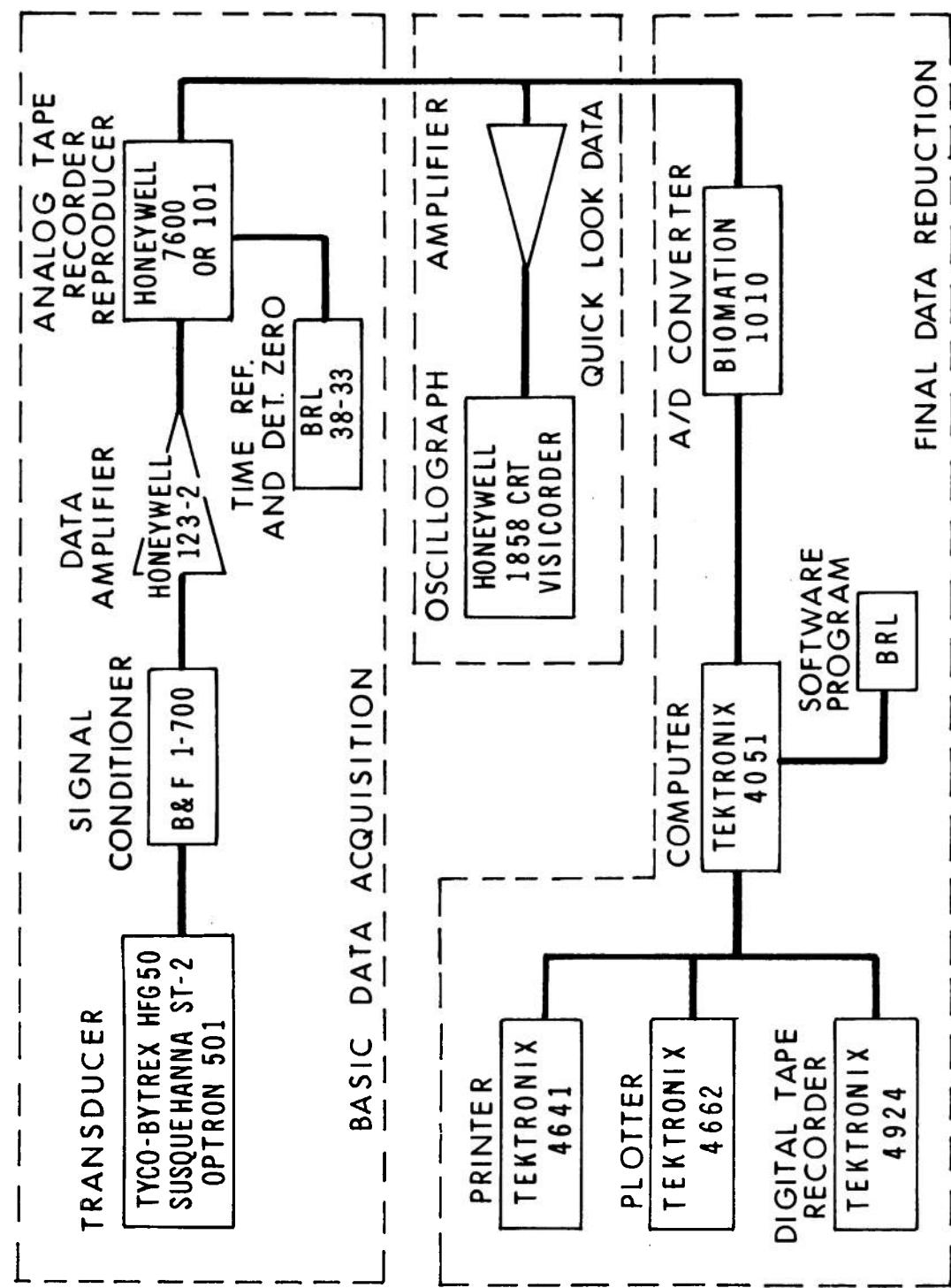


Figure 4. Schematic of data acquisition-reduction system.

III. RESULTS

Test results are shown in Figure 5. The upper trace indicates the pressure load as it was applied over the top of the TM-46/MVM mine-fuze combination. The lower trace shows the corresponding displacement of the movable fuze body as mounted in the top of the mine.

The lower trace has indicated on it where the fuze was activated. The time was measured from the vibration pick-up record (not shown). It is the time from the initial pressure load is begun until the fuze firing pin is released under fuze activation. The vibration signal from the activation was picked up by the ST-2 sensor attached to the mine body.

The next section describes a way to combine the two load and deflection records just described.

IV. ANALYSIS

A useful way to present the test data to be used in a numerical model is in a combined deflection-load curve. To do this, it is necessary to combine the digital output from the pressure (load) and deflection monitors. Table I gives such a listing for several time steps taken from the test records. The fuze activation is noted in the table.

The force applied to the sensitive top surface of the mine during the test was calculated by taking the projected area of the top (0.0699 m^2) and multiplying by each pressure increment in the table. A cross-plot of the resulting loads and deflections was then made. Figure 6 is this cross-plot. Again, the point of fuze activation is noted at 3.29 kN for a displacement of 1.93 mm.

V. SUMMARY AND CONCLUSIONS

A method has been described for static loading of irregular sensitive surfaces of anti-tank mines. A load-deflection curve for a mine-fuze combination can be obtained by use of this method. Such a curve is helpful to establish a numerical model to be used in an assessment of a mine's vulnerability.

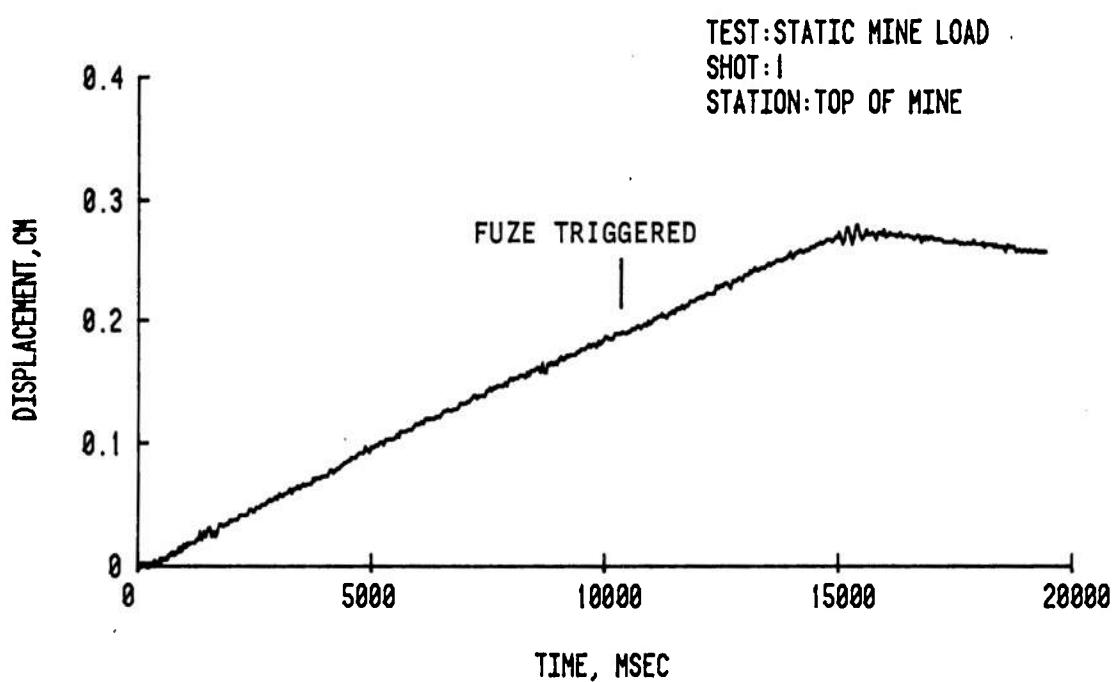
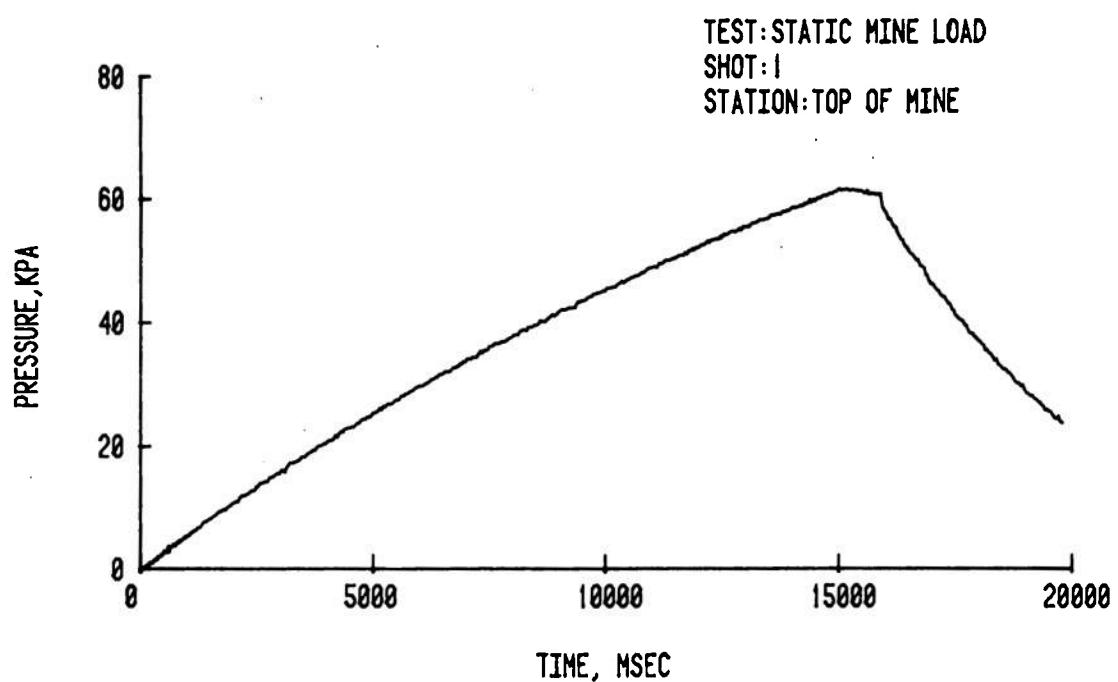


Figure 5. Pressure and displacement curves.

Table I. Deflection-Load Parameters for the TM-46/MVM Mine-Fuze Combination

<u>Pressure, kPa</u>	<u>Force, kN</u>	<u>Deflection, mm</u>	<u>Time, ms</u>
0	0	0	0
2.88	.201	.08	500
5.55	.388	.19	1000
8.22	.574	.29	1500
10.89	.761	.42	2000
13.36	.934	.50	2500
16.03	1.120	.59	3000
18.49	1.292	.69	3500
20.75	1.45	.76	4000
23.22	1.62	.90	4500
25.28	1.77	1.01	5000
27.74	1.94	1.09	5500
29.80	2.08	1.20	6000
32.06	2.24	1.26	6500
34.11	2.38	1.38	7000
35.55	2.48	1.45	7500
38.02	2.66	1.55	8000
39.87	2.79	1.64	8500
41.92	2.93	1.72	9000
43.56	3.04	1.76	9500
45.41	3.17	1.85	10000
47.06*	3.29	1.93	10410
47.26	3.29	1.93	10500
49.11	3.43	2.04	11000
50.76	3.55	2.12	11500
52.40	3.66	2.22	12000
54.04	3.78	2.33	12500
55.69	3.89	2.41	13000
55.89	3.91	2.50	13500
58.77	4.11	2.58	14000
60.00	4.19	2.64	14500
61.85	4.32	2.77	15000
61.24	4.28	2.71	15500
57.74	4.04	2.71	16000
51.58	3.61	2.71	16500
46.24	3.23	2.67	17000
41.10	2.87	2.64	17500
36.78	2.57	2.62	18000
32.47	2.27	2.60	18500
28.56	2.00	2.56	19000
25.28	1.77	2.56	19500

NOTE: (1) Force calculated for $.0699 \text{ m}^2$ of top area of mine (11.75 in. dia).
 *Fuze triggered.

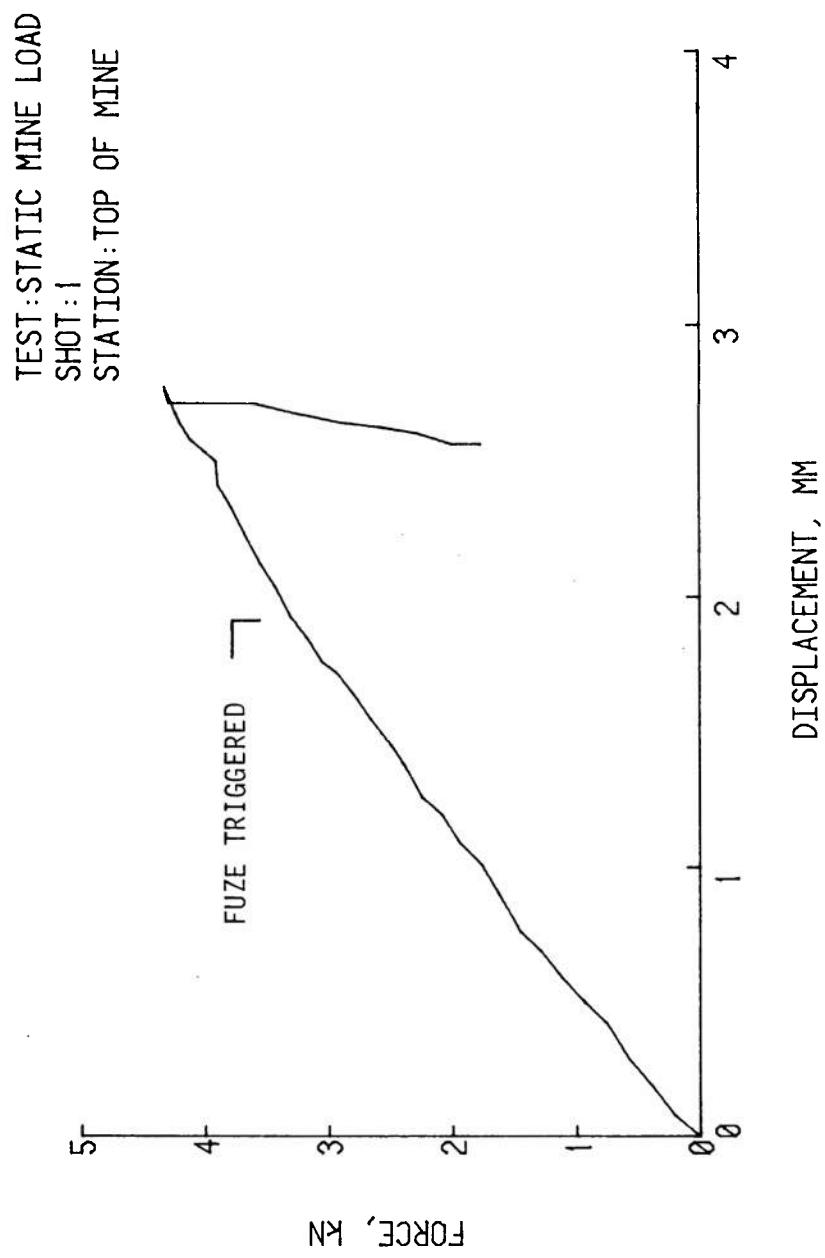


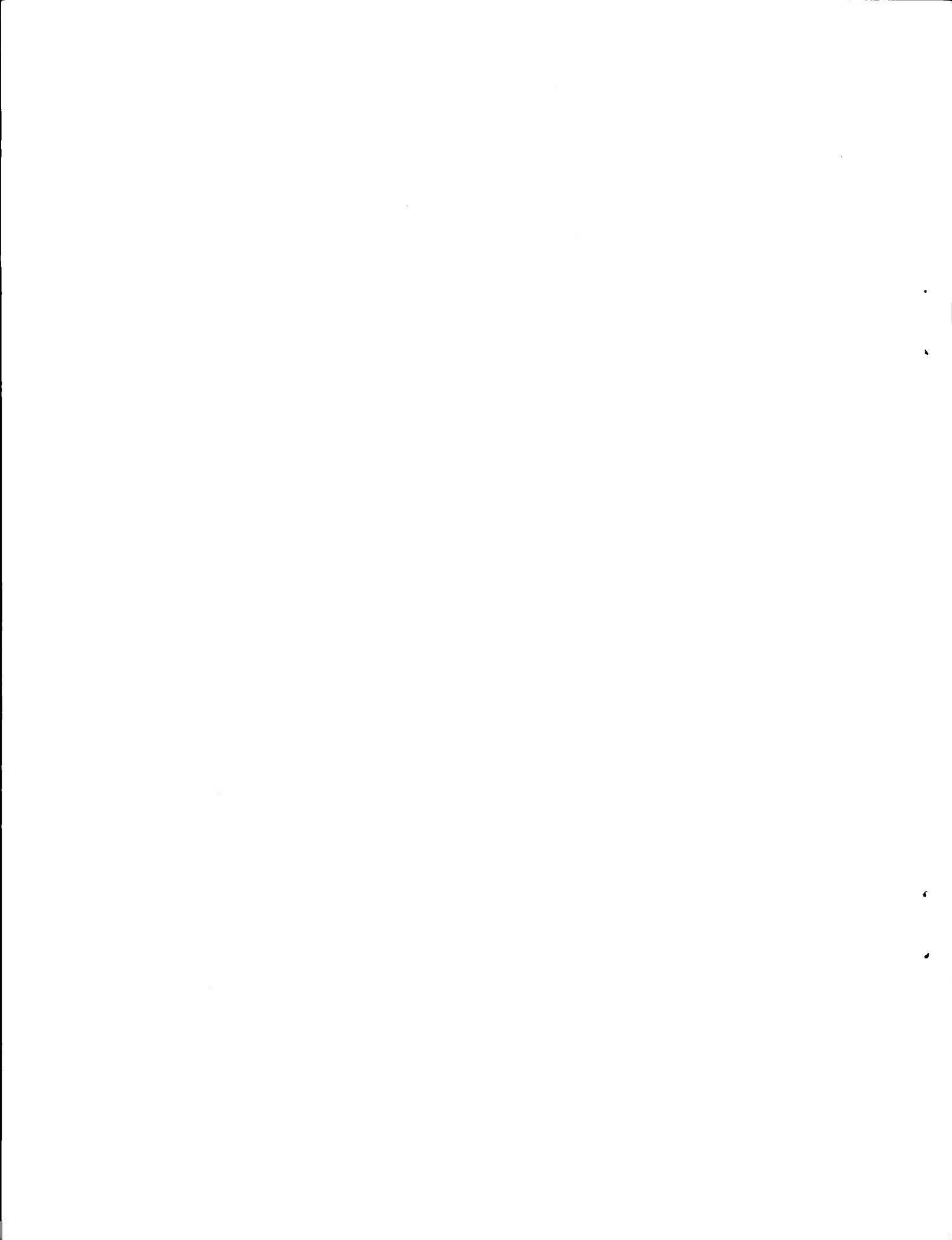
Figure 6. Force-displacement curve.

An example was presented for the TM-46/MVM mine-fuze combination. A load-deflection curve was developed and presented for this combination. The loading test showed fuze activation for the combination at 3.29 kN (47.0 kPa, 6.82 psi) force at 1.93 mm (0.075 in.) deflection.

Generally, the loading procedure is quite simple and uses available off-the-shelf equipment. The static test chamber is easily converted back to a shock tube (after static use) for the dynamic portion of the vulnerability assessment.

ACKNOWLEDGEMENT

The authors wish to thank Mr. Charles Kingery for his most helpful discussions during the development and use of the static load generator.



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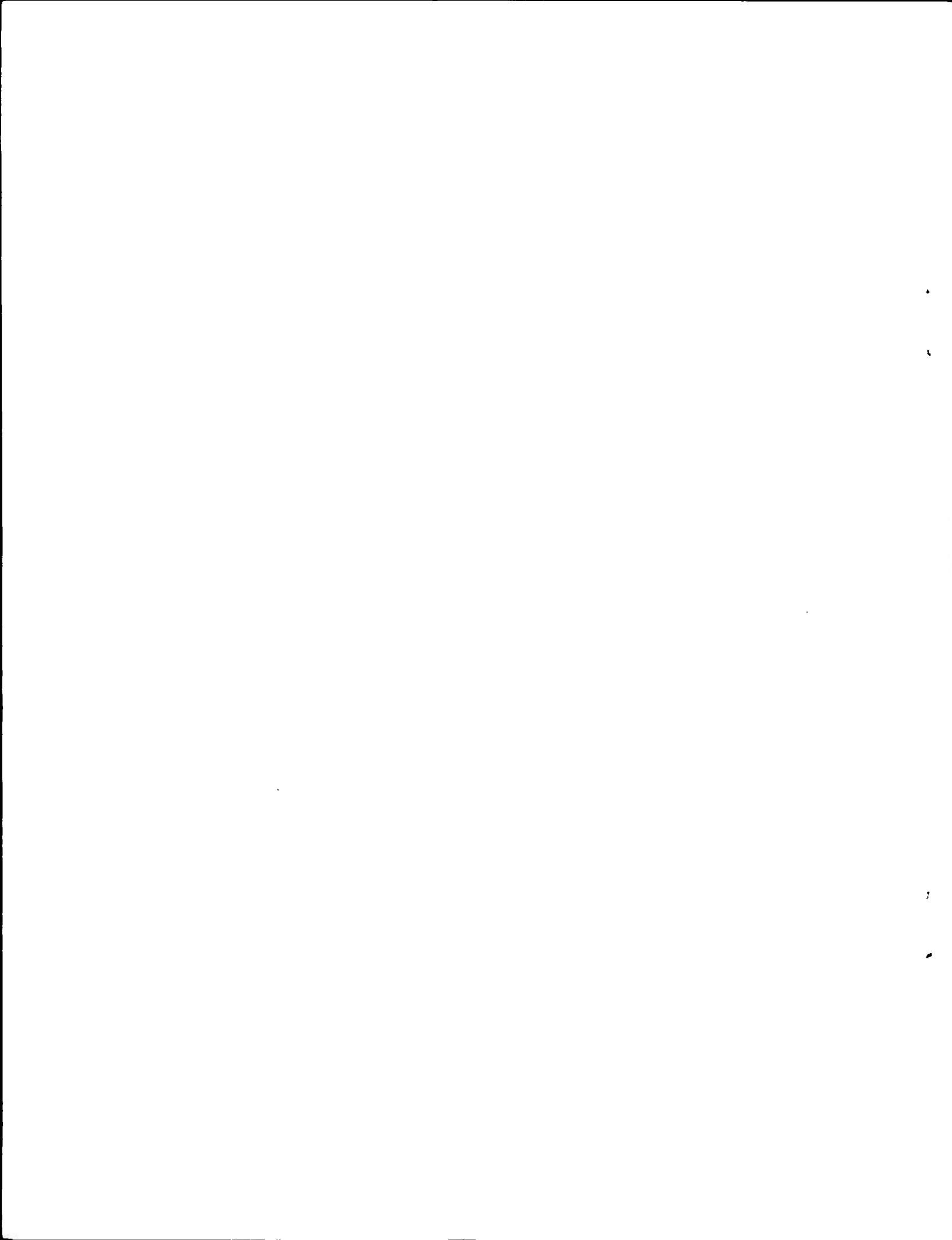
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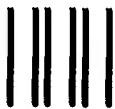
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